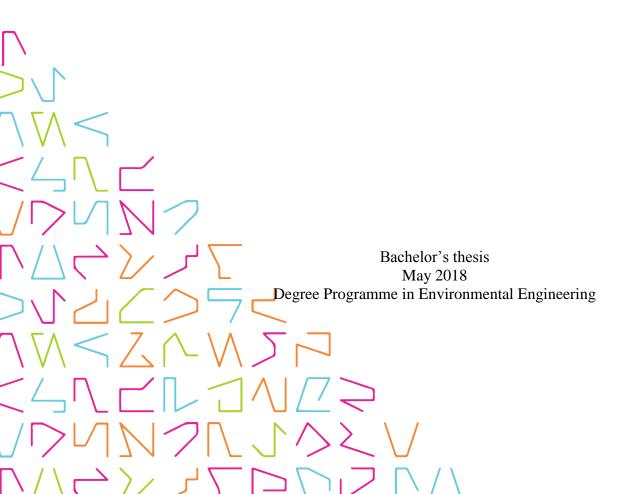


HBCD IN INSULATION MATERIALS

XRF in Preliminary Detection

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ABSTRACT

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Due to a new amendment to a piece of legislation on persistent organic pollutants, consistent methods are needed to properly detect, process and dispose of a newly added substance, hexabromocyclododecane, which has now been globally banned from use.

Bromine based flame retardants like HBCD have been used increasingly in construction materials since the 1960s to meet fire safety requirements, so it will be widely present in demolition waste in the years to come. HBCD has been used especially in insulating materials such as expanded and extruded plastics, but it could also be present in imported packaging materials of electronics and other products. No samples of packaging materials containing HBCD were found during this study.

Hexabromocyclododecane (HBCD) cannot be visually detected, nor has it been marked or labeled on the products it has been used in. Because chemical laboratory analyses to detect HBCD are time-consuming and the volume of construction waste considerable, a faster on-site method is needed.

An x-ray fluorescence gun can detect bromine from plastics. Because HBCD contains bromine, XRF can be used to estimate whether HBCD could be present, although the results are not conclusive enough to replace more accurate laboratory analyses entirely.

The method described in this thesis work appears to be suitable for identifying materials that have not been treated with any brominated flame retardants, but additional steps need to be taken to tell HBCD apart from other brominated compounds.

Key words: detection method, construction waste, polystyrene, hexabromocyclododecane

CONTENTS

ABBREVIATIONS AND TERMS

Br	bromine
EPS	expanded polystyrene
FR	flame retardant
GC	gas chromatography
HBCD	hexabromocyclododecane
PBDEs	polybrominated diphenyl ethers (flame retardants)
PBT	persistent, bioaccumulative and toxic substance
PolyFR	copolymer of styrene and butadiene, new flame retardant
POP	persistent organic pollutant
SYKE	Finnish Environment Institute
TBBPA	tetrabromobisphenol A (flame retardant)
UNEP	United Nations Environment Programme
XPS	extruded polystyrene
XRF	X-ray fluorescence

1 INTRODUCTION

A decision made by UNEP Stockholm Convention in 2013 listed hexabromocyclododecane as a persistent organic pollutant (POP), and it was subsequently banned globally. (UNEP SC-6/13, 2013)

HBCD has been used as a flame retardant in construction and insulation materials, and continues to exist in buildings approaching their end of life. To assess the implications of the Stockholm Convention decision on how waste insulation materials from demolished buildings are processed and disposed of, two study departments of Tampere University of Applied Sciences formed a preliminary 4-thesis-project with Finnish Environment Institute SYKE.

The goal of the whole project is to provide background information and material for instructions for construction workers, builders and authorities on how to detect, separate and process HBCD from construction waste.

This paper focuses on on-site detection of bromine as an HBCD indicator by using a handheld x-ray fluorescence gun. The goal was not to accurately measure the amount of bromine or HBCD present, but to simply find out whether the presence of HBCD was possible to predict with this method or not.

2 BACKGROUND

2.1 HBCD and Brominated Flame retardants

Hexabromocyclododecane, or HBCD, is a bromine-based flame retardant that has been widely used since the 1960s to reduce the flammability of otherwise flammable materials, particularly insulation materials made of polystyrene.

Polystyrene foam (EPS and XPS) is an affordable and versatile plastic used to insulate buildings to prevent unwanted heat exchange. It is easily shaped into any form it is needed in and resists moisture, but flame retardants such as HBCD have been used to allow buildings to meet fire safety regulations. (Plastics Europe, 2014)

Although HBCD has now been classified as a persistent organic pollutant and banned from use (Ympäristöhallinto, 2018), some other brominated flame retardants, such as HBCD's newer replacement, a butadiene styrene brominated copolymer PolyFR, can still be used. (EPA, 2014; Schlummer et al., 2015)

The difference between the banned brominated flame retardants and the still allowed ones is the way they are used in the polystyrene resin. Many of the banned substances like HBCD and PBDEs are *additive*, while the others (PolyFR and TBBPA) are *reactive*. Reactive flame retardants are covalently bonded with the polystyrene and are therefore less likely to get separated from the insulation material into the environment than the more easily extractable additive ones. (Hyötyläinen, 2002)

2.2 Properties

According to its material safety data sheet (MSDS), HBCD is a persistent, bioaccumulative and toxic substance (PBT) with the molecular formula of $C_{12}H_{18}Br_6$ and molecular weight of 641,73g/mol.

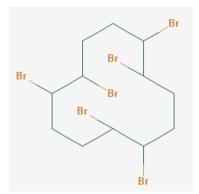


Figure 1. Structural formula of HBCD (PubChem, 2018)

On its own, HBCD is a white powder, but when it is mixed in as an additive with the polystyrene resin, it has no apparent colour or smell and can only be detected through chemical analysis, such as gas chromatography.

HBCD is very toxic to aquatic life with long lasting effects and presents a hazard to humans and animals as an endocrine disrupting chemical. It is toxic to the thyroid and liver, and appears to cause developmental problems in infants. (Papaspyrides & Kiliaris, 2014)

Because of the large volumes of FR treated plastics in construction waste, and because HBCD persists in nature and travels long distances once attached to airborne particles, it is a formidable and long-lasting environmental pollutant. (Ympäristöhallinto, 2018)

While EPS and XPS insulation materials that do not contain HBCD can be readily recycled, any materials treated with HBCD should be disposed of by incineration in a wellfunctioning waste incineration plant under high temperatures (Plastics Europe, 2014).

2.3 Occurrence

According to SYKE, around 10% of the EPS used in construction is treated with a fireretardant chemical. (Seppälä, 2016)

Another thesis in this project covers the occurrence of HBCD in buildings in Finland. (Hämäläinen, 2017)

2.4 Detection

Over the course of the project it has become clear that accurate data on where and how frequently HBCD has been used in construction materials are not readily available. Detecting it to be able to process the waste correctly is important – while polystyrene in general is recyclable, any polystyrene that contains HBCD should be handled with appropriate caution and disposed of by incineration.

In a laboratory setting, HBCD can be measured directly using different kinds of gas chromatography (GC) methods. A separate thesis work is to be published on the specific laboratory analyses.

To indicate presence of HBCD quickly and on site, however, an x-ray fluorescent gun (XRF) can be used to measure the amount of bromine in a plastic product or insulation material. Each HBCD molecule has six bromine atoms, which the XRF can pick up on.

If the reliability of an XRF method can be shown, using a handheld XRF-gun for screening waste materials would be faster and more practical than sending samples of all construction waste polystyrene directly to laboratory analyses when use of HBCD is suspected.

3 MATERIALS AND METHOD

3.1 XRF

The device used in both screening and radiation laboratory analysis of this study was a Thermo Scientific Niton XL3t GOLDD handheld XRF analyser. The calibration configuration used was Consumer Goods: Plastics.



FigureX. Niton XL3t GOLDD XRF Analyzer. (ThermoFisher Scientific)

Although the purpose of this thesis was to estimate the presence of HBCD in the collected samples, the device produces an elemental analysis and therefore measures bromine in Br ppm, not HBCD directly.

To analyse the samples measured, and to control the XRF in its table stand remotely, two pieces of compatible computer software were used: NDT 7.2.2. and NDTr 7.1.2.

Samples were collected from three separate source categories (A, B and C). Two of the three sets went through an additional screening phase to selectively reduce the amount of material.

There were two initial goals behind the sample selection: to map out what kind of sources HBCD could be found in, and to see how accurately a hand-held XRF analyser could predict its presence in the sample.

To that end, finding samples with bromine was prioritized.

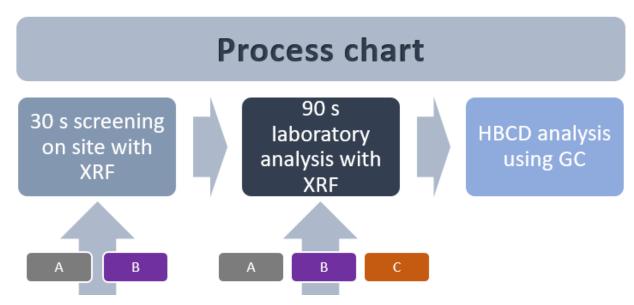


Figure 2. Process flow in this study

The samples were collected and screened, and the selected samples bagged and labelled on site. Some of the samples that were found to contain no bromine in the screening were discarded.



Figure 3. Sample A9. Light blue XPS.



Figure 4. Discarded sample A15. White EPS.

3.2.1 Sample set A

The first set of samples (A) was randomly selected from a local construction waste stream. The collected samples went through the additional screening step on site to determine which samples would be taken to the radiation laboratory for further analysis.

From this source, the intention was to collect samples that appeared to contain bromine in levels high enough to indicate presence of HBCD. The material in the waste stream was mainly construction waste, some from older demolished buildings, so this was considered to be the batch most likely to contain samples treated with HBCD.

Because these samples were collected from a unified waste stream, it is not possible to pinpoint where exactly each individual sample originated from.

3.2.2 Sample set B

The second set (B) consisted of packaging materials of everyday items, furniture and electronic appliances, collected by various people involved with the project, from a variety of different sources.

The intention was to collect information on what kind of packaging materials HBCD might be present in.

These samples were also screened before selection for the laboratory analysis.

3.2.3 Sample set C

The third set (C) was collected from a current local construction and renovation project of an apartment building, and include insulation materials as well as packaging materials for home appliances. To select samples for the laboratory analysis, a quick 30-second XRF screening was done on site to determine which samples would be included in further analysis to avoid collecting only samples with no bromine present in them, or only samples with large amounts of bromine.

Each sample (from sets A and B) was measured for 30 seconds, 10 s with each filter of the handheld XRF. Due to the large amount of available material, most of the samples that appeared completely free of bromine in the screening were discarded. A few were kept to provide a reference point for the analysis.

3.4 Radiation laboratory analysis

The actual analysis of the selected samples was carried out in a radiation laboratory, using a table top stand for the handheld XRF machine.

The duration of each measurement was set to 90 seconds, 30 seconds with each filter. Because the XRF only measures a small area on the surface of the sample during each measurement, each sample was measured three times and the average result calculated from all three.

When possible, the sample was cut in half and one or two of the measurements done from the freshly exposed surface to avoid only measuring the dirtier surface layers that could have been in contact with HBCD or bromine and give a positive reading even if no brominated flame retardants were used in the material itself.



Figure 5. Radiation laboratory equipment setup.

3.5 Comparison

Simultaneously with the radiation laboratory measurements, a parallel testing was conducted in the chemical laboratory using gas chromatography.

It is important to note that unlike the XRF, the chemical analysis directly measures HBCD instead of bromine as an indicator. This means, for instance, that 1000 ppm Br measured with the XRF analyser is not the same result as 1000 ppm HBCD measured with GC.

While the results of the two types of measurements are not directly comparable, the presence or absence of presumed HBCD can be indicated by either method.

The last column in Table 1 (section 4.1.2) shows the preliminary result of the chemical analysis.

4 MEASUREMENT RESULTS

4.1 Results of radiation laboratory analyses

The data from the screening, the actual XRF measurement and the GC measurement done in the chemistry laboratory were collected in one table (Table 1). The errors as they are reported are due to the detection properties of the equipment used.

4.1.1 Errors

The errors of the XRF screening are not presented. The screening was done solely to select samples, not to produce accurate and comparable results. These results are presented in the table only to depict the difference between the 30 second screenings and the actual 90 second measurements.

The average error of three measurements of the 90 second XRF analysis is marked in "Br error (of 3)" column.

The error for the analyses done in the chemistry laboratory is approximately 10%. The full thesis on the GC analysis with its exact error values is yet to be published at this time.

4.1.2 Results

Table 1. Colour	coded table	of results.
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SAMPLE	Description	Br 30s ppm	Br 90s Avg ppm (of 3)	Br Error (of 3)	ppm HBCD, mg/kg
A1	White EPS	194	670	59	none
A2	Pink foam, hard	2261	2627	110	3200.0
A3	Grey EPS	7197	6266	322	none
A4	Grey EPS	5759	6682	299	none
A5	Grey EPS, smaller grainsize	6513	7415	173	none
A6	Grey EPS	0	0	31	none
A7	White EPS	724	302	43	none
A8	Grey EPS, smaller grainsize	7020	6699	279	-
A9	Light blue XPS	10900	9456	298	15000(-25000)
C1	Yellow XPS		0	16	none
C13	Insulation material		261	42	none
C14	Underfloor insulation, grey		50	16	none
C15	Underfloor insulation, current construction, grey		7845	290	none
C17	Underfloor insulation, current construction, grey		7372	308	none
C18	Socle EPS, current construction		3215	171	none
C19	Underfloor insulation, grey		7178	279	150-300
C20	Underfloor insulation, socle		5902	246	none
C21	Underfloor insulation, socle, white		5879	243	none
B1	Chinese souvenir packaging	0	0	66	none
B2	Couch structure packaging	3467	3265	164	-
B3	Clock radio packaging	0	0	22	-
B4	Packing peanuts, compact	77	401	75	-
B5	Packing peanuts, porous	0	0	33	-
B6	Packing peanuts, yellow	89	440	77	-
B7	Television packaging	0	0	42	none
C2	Dishwasher packaging		179	26	-
C3	Refridgerator packaging		0	69	-
C4	Stove packaging		33	25	-
C5	Dishwasher packaging		0	29	-
C6	Refridgerator packaging, from Hungary		0	32	-
C7	Microwave packaging, from UK		0	29	-
C8	Stove packaging, from Germany		0	32	-
C9	Induction stove packaging, from Germany		0	57	-
C10	Refridgerator packaging		0	72	-
C11	Laundry machine packaging		0	32	-
C12	Induction stove packaging, from Germany		0	31	-
C16	Television packaging, from Hungary		0	122	-

Red highlights in the table depict samples where HBCD was initially estimated to be present and green highlights samples presumed free of HBCD based on initial assumptions, in cases where both an XRF measurement and a lab measurement have been done for the sample. The samples in the above table have been sorted by type: first waste materials, then construction materials and finally packaging materials.

5 DISCUSSION

5.1 Observations

Based on the data presented in this thesis work, the following observations can be made:

- 1. HBCD occurs in demolition waste insulation materials in Finland.
- 2. HBCD was not found in packaging materials in this study.
- 3. XRF does detect bromine in all samples containing HBCD.
- 4. XRF does not differentiate HBCD from other bromine-based compounds.

The table of results (4.1) shows that the XRF gave more positive results (bromine detected) than the chemical analysis (HBCD detected), which confirms that the XRF cannot differentiate between HBCD and whatever other chemical compound or flame retardant might have been used.

In this study XRF did, however, produce a result other than zero for all the samples which contained HBCD according to the laboratory analysis. This suggests that the method described in this paper *is* one way of identifying and excluding insulation materials that have not been treated with brominated flame retardants at all.

Although the XRF-measured presence of bromine might indicate use of some brominated flame retardant, it does not detect the molecular structure. In other words, it measures bromine whose presence suggests that a brominated flame retardant has been used, but a further chemical analysis needs be done to identify the specific FR used.

5.2 Accuracy and reliability

The initial assumption was that based on the XRF results, a 'limit value' of Br ppm could be given as a result of this study, to easily tell whether the sample contains HBCD or not based on the amount of bromine in the sample. The laboratory-confirmed results, however, show that HBCD was found in samples with Br ppm ranging from as low as 2600 up to almost 10000. Some samples whose measured results were in the middle of that range did *not* contain HBCD when measured with gas chromatography, so the idea of such a limit value is not feasible.

One possible reason for the largeness of the range of measured Br ppm is that different kinds of brominated flame retardants and their various derivatives have been used over the years, on insulation materials of varying compositions. (Hyötyläinen, 2002) Differences in the amount of retardant used on the product, as well as in the product material itself, affect the measured XRF results.

It is worth consideration that if the exact amount of Br ppm does not give any additional information or insight, only its presence or absence in the sample is significant, and the results should be considered qualitative estimates instead of quantitative analyses. This reduces the accuracy required from the method, and shorter measurement times might suffice for field measurement purposes in the future. During the measurements done for this thesis, for instance, the XRF quickly showed if the amount of bromine in the sample was below detection limit when none would be found, and did not deviate from that reading over the measurement time.

A related conclusion was drawn in a study done by Washington State Department of Ecology in 2012. While the study focused on PBDEs rather than HBCD, it approached the matter by using XRF to screen for bromine as an indicator of a brominated flame retardant as well. They found that the method has a tendency to give 'false positives' - samples with bromine detected in the absence of PBDEs. (Furl et al., 2012)

False positives, however, are not as problematic as 'false negatives'. Samples that did not contain bromine according to the XRF measurement in the study mentioned above did not contain PBDEs in more accurate and specific laboratory analyses either, so the potential downside in using this method is only in having to send negative samples to be analysed further in the case of a false positive reading.

5.3 Further studies

While the method described in this thesis work seems to accurately indicate the presence or absence of brominated flame retardants in general, it does not offer the means to differentiate between specific banned (HBCD) and currently legal flame retardants. The new alternative to HBCD, PolyFR (Beach et al., 2013), and another popular brominated FR, tetrabromobisphenol A (TBBPA) (EPA, 2014; Lüthje, 2003), also contain bromine and will turn up in measurements using the method described here.

A study on the same topic as this thesis work, published in Germany in 2015, solved this problem by adding an extra step of dissolving a portion of the sample in acetone. The idea behind the extraction step is that both PolyFR and TBBPA are *reactive* retardants and form chemical bonds with the polystyrene, whereas HBCD is *additive* and can be separated from the insulation material when dissolved in an acetone solution. (Schlummer et al., 2015)

A chart of a suggested improved process flow for future studies is depicted in appendix 1. In it, the first XRF measurement is taken directly from the polystyrene sample. If the sample contains no bromine, no brominated flame retardants have been used and the material can be recycled. If, on the other hand, it does contain bromine, an extraction can be done to a portion of the sample. The sample is then dissolved in an acetone-based solution, and the next XRF measurement taken from the extraction solution. If the bromine can now be found in the extraction solution, the sample most likely contains an *additive* retardant such as HBCD. If the bromine remains in the polymer gel after extraction, it is likely to be bound to a *reactive* FR such as PolyFR or TBBPA.

The next proposed course of action is to test the extraction method and its viability as an on-site method by comparing its results to chemical analyses, and creating step-by-step instructions for a suitable field detection method. Due to the commercial availability and relative harmlessness of the materials needed for the extraction, it might be possible to eventually piece together a measurement kit for on-site detection, with solvent measured beforehand, a scale to weigh the polystyrene sample, and suitable containers for dissolving it.

This way, only the samples with bromine measured from the extraction solution would have to be sent to the laboratory for GC analysis.

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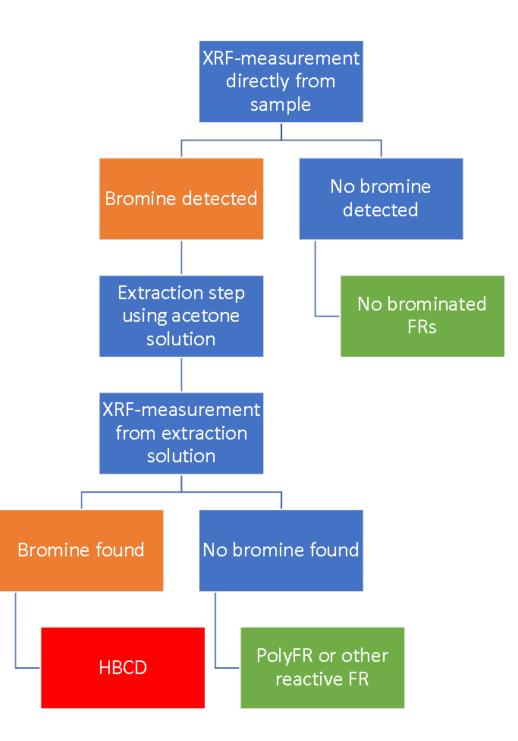
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APPENDICES



Appendix 1. Suggested method flow chart with extraction step

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8 9 8 8 8 8 8 9 ₽ 14.79 21.04 11.85 17.75 20.14 28.62 26.68 21.05 22.41 18.85 12.52 14.4 17.17 25.41 20.14 15.97 18.87 29.41 12.53 14.32 27.49 13.51 18.13 24.58 20.9 21.4 18.87 8. 22 8.36 16.71 20.19 26.37 33.95 19.42 14.1 32.84 Ж 15.2 19 As Error ä 01 × 007 v < LOD 007 v QD^∧ 00 ~ 00 ~ 00 > 00~~ 9 00 V < LOD 8 8 8 3 9 8 9 9 8 9 9 9 8 9 8 8 8 8 8 8 8 116.05 < LOD 8 8 9 8 8 As 83.15 < 1 35.9 < 17.13 38.53 45.07 43.39 35.2 52.14 72.92 43.14 17.87 40.53 41.14 45.34 41.23 22.95 96.74 45.97 47.53 82.92 8 25.7 8 67.74 43.99 30.54 5 8 8 8 3 В 8 42 8 К 8 \$ Se Error 5 42 8 6 8 Ř 24 ä ដ 4 Ϋ́ς ģ ਸ਼ੁਂ ŝ 8 007 > 007 Q0) × 8 8 8 8 8 8 8 8 8 8 8 8 9 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 9 8 8 8 8 š 109.36 301.13 270.39 197.49 36.35 43.06 50.12 260.17 284.48 359.67 291.47 241.63 59.24 159.03 165.46 68.11 32.65 95.71 103.47 309.4 28.45 27.19 293.6 72.22 66.58 167.72 20.65 22.41 22.55 89.38 47.84 354.67 .66.9 156.07 37.29 67.77 8 Error 117. 327 251 9604.41 412.76 1650.63 6592.43 6363.16 7638.24 6950.68 423.86 9299.15 9464.96 3253.32 3268.69 198.07 2912.35 2230.37 5843.87 207.74 6845.38 6696.91 6555.31 3272.13 389.36 6882.03 6606.62 6558.64 162 7656.5 275.3 737 8 8 8 8 8 8 8 8 8 8 33.43 32.05 22.83 39.45 42.12 42.48 38.47 42.13 18.35 18.55 27.09 31.25 24.14 19.34 23.13 23.94 27.93 36.11 36.54 25.83 26.29 35.49 32.56 47.46 30.79 17.63 22.35 32.26 21.91 30.67 60.7 35.92 42.58 32.6 37.87 33.32 17.81 38.91 29.5 Pb Error 50.17 QD ×LOD Q0,× 0Ĵ^ Q0]∨ <10D 00 1 9 907~ °_0 Q0, 9 00 1 9 007× °L0D 07 0<u>0</u> 00 V 0 00 V 0J^ <10D 00 1 <l>COD 0J 1 0<u></u> 0<u>0</u> 07 0<u></u> 00]v Q0√ ×LOD 0 1 2 ¢L0D 0)^ 9 132.13 < LOD 60.15 < LOD £ 149.26 161.6 115.22 178.45 135.56 L00.35 29.78 26.35 23.76 37.83 39.25 136.04 120.63 142.39 97.08 39.73 98.35 101.94 65.6 73.45 142.11 123.4 79.02 73.93 24.44 22.6 20.65 42.45 40.04 33.17 80.97 63.47 48.58 41.64 98.57 59.25 72.72 BiError 907 ۲OD ۲ 0 V 9 COD 9 4 LOD 97 0, 0, 00 V 9 ĝ 9 Q01× COD 00 V 8 8 8 8 8 8 8 8 8 8 9 9 8 8 8 9 8 1216.36 < LOD 9 8 8 窗 729.3 < L 781.23 839.27 724.78 816.15 709.9 I 1028.14 750.64 320.85 476.95 750.64 794.57 - 60°098 734.64 623.96 568.73 741.54 799.57 809.59 675.64 682.99 1152.71 ß 1203.1 874.89 1330.01 44 46 45 ଷ୍ପ 17 99 B 8 99 8 ដ ß **Bal Error** 1021.0 1726.0 1398. 1144.0 1188 766. 718. 8 767. 33. 827 723. 1392. 992000.19 992423.19 998253.19 993514.88 999134.44 975684.19 991866.75 990896.63 99.2515.69 945779.19 969730.69 979795 996824.63 998624.25 994492.56 991922 989255 990940.25 991438.88 996400.94 995416.63 8 995375.88 53 8 8 90.2799.06 8 998289.19 998092.19 8 998670.63 56 992511.38 997174.25 998825.75 987462 993789.5 996085.06 2 2602 66 984354.6 991187.0 998291.(998262.5 997078. 983947. Bal 75.43 52.65 37.53 41.16 68.08 52.29 54.02 44.96 31.23 64.34 52.64 49.85 55.66 55.83 74.02 51.97 44.08 49.06 35.88 25.08 75.15 82.88 84.76 49.46 57.03 76.46 77.49 70.61 Cd Error 30.88 58.11 21.81 31.91 45.39 49.23 52.07 53.7 23.87 53.97 43.6 8 З 68.12 112.54 63.32 69.46 65.6 27.14 65.72 90.73 71.94 55.78 46 82.85 69.03 72.41 72.54 98.9 55.85 63.54 43.73 40.64 31.54 94.42 62.28 91.68 46 ŝ ŝ 30.04 65.85 104.07 Я 57.41 8 4 50.2 27.11 56.91 49.91 61.37 Sn Error 5 8 ŝ ŝ 8 5 ŝ 49.93 0 1 0 1 ۲00 ۲ 8 8 8 < LOD 9 8 8 8 9 8 8 9 8 8 8 9 8 9 9 8 8 9 8 8 8 8 9 8 8 8 9 8 9 8 8 S 102.15 < 1 94.14 < l 131.32 < l v 115.47 96.15 144.16 161.19 106.84 141.42 95.52 53.88 72.26 99.12 102.37 132.31 94.74 105.64 80.24 43.13 39.55 58.44 103.26 8 78.76 89.85 63.05 . 45.36 139.62 157.47 92.71 104.01 83.54 83.93 90.83 138.31 141.02 ß 8 Sb Error 8 100 Ę. 101 340.58 < LOD â 9 76 < LOD 276.88 < LOD 9 353.93 < LOD 0 261.69 < LOD 145.64 < LOD 001 > 69" < LOD L.5 < LOD ŝ 36 < LOD 8 8 8 8 8 Ω0 ρ Ő 519.24 < LOD 346.73 < LOD 204.84 < LOD 185.63 < LOD 369.68 < LOD 503.54 < LOD 562.06 < LOD 460.32 < LOD 449.41 < LOD 204.49 < LOD 180.82 < LOD 598.53 < LOD 8 8 483.59 < LOD 8 ß 262.54 < 517.15 244.72 < 323.46 < 472.54 < 342.49 515 288.99 453.01 461.77 418.67 525.31 593.46 315.21 355.67 291.08 514.93 Error 263.1 521 513. 521. B В 455.5 813.5 946.3 29 418.24 2 ß В 4 ß ß 2 8 49 ŝ ន Ж 74 33 87 52 87 47 77 457 1483.(1341.(1593.4 1308.7 80 717 545. 332 6 475. 1225 575. 8 -54 798. 550 641. 27 634 976 8 8 8 8 8 8 8 8 8 8 8 1297 8 8 B A01-2 A03.2 A07-2 A08.2 A08.3 A09.3 A11-2 A11-3 B04.3 B07.3 A01-3 V05-2 V06-3 A07-1 A07-3 A11-1 A13-2 B01-2 B01-3 B07.2 A01-1 V05-3 406-2 A13-1 413-3 801-1 B04.2 306.3 403.3 406-1 B04.1 B06.2 8 1651 409.2 B07.1 8 100 B06.1 ud đ шd 없 шd đ đ ۵ mqq шd đ ۳qq mqq шd ۳ ۳qq шd mqq đ mqq đ ۳qq ᇟ mqq 섮 섮 đ Juits d ଘ шd ᇟ шd 덦 섮 шd шd d 덦 d 8 8 8 8 8 8 96 8 6 8 8 6 8 6 6 6 8 8 6 8 8 8 8 6 6 6 6 6 8 8 8 6 6 8 8 6 8 8 8 Jurati

Appendix 2. Data from XRF measurement

2	User Logi <mark>Ba</mark>	Ba Error	ą,	Sb Error	s, us	Sn Error C	3	Cd ErrorBa		Bal Error	18	BiError	æ	Pb Error	Br	Br Error	s	Se Error	As I	As Error	Hg
B08.1 <	4 LOD	546.53	<pre>COD </pre>	102.38	qo⊺≻	68.22 <	00 × 10D	53.55	996156	820.59	Q07⊁	35.88	dol>	24.38	< LOD	31.76	QD ≻	44.34	< LOD >	17.87	4 LOD
B08.2	579.24	4 327.08 < LOD	<pre>COD </pre>	95.36 < LOD	< LOD	62.84 < LOD	ίου	49.23	997391.44	760.46 < LOD	< LOD	28.19	28.19 < LOD	21.27	< 10D	26	< LOD	37.09 < LOD	< LOD	16.56 <	< LOD
B08.3	820.23	8 418.91 < LOD	<pre>COD</pre>	120.45 < LOD	≺LOD	75.28 < LOD	τοD	63.06	996608.88	977.26 < LOD	< LOD	35.96	35.96 < LOD	22.74	< LOD	42.12	4 LOD	58.54	< LOD	19.33	< LOD
B09.1	1362.43	3 577.94 < LOD	< LOD <	160.94 < LOD	qol≻	117.52 < LOD	ίου	88.01	991471.25	1331.5 < LOD	< LOD	81.79	81.79 < LOD	42.87	366.78	80.15	< LOD	111.55 < LOD	< LOD	35.57 < LOD	TOD
B09.2	982.36	6 451.97 < LOD	< LOD <	123.29 < LOD	<lod< td=""><td>83.66 < LOD</td><td>ίου</td><td>75.78</td><td>994784.06</td><td>1064.94</td><td>< LOD</td><td>44.62</td><td>roD</td><td>37.16</td><td>503.25</td><td>67.2</td><td>< LOD</td><td>72.08 < LOD</td><td>< LOD</td><td>24.55 <</td><td>< LOD</td></lod<>	83.66 < LOD	ίου	75.78	994784.06	1064.94	< LOD	44.62	roD	37.16	503.25	67.2	< LOD	72.08 < LOD	< LOD	24.55 <	< LOD
B09.3	1806.07	576.61	< LOD	156.46	<lod< td=""><td>108.17</td><td>< LOD</td><td>87.59</td><td>994509.44</td><td>1340.41</td><td>< LOD</td><td>77.83</td><td><lod< td=""><td>53.31</td><td>450.34</td><td>83.91</td><td>< LOD</td><td>109.36</td><td>< LOD</td><td>39.25</td><td>< LOD</td></lod<></td></lod<>	108.17	< LOD	87.59	994509.44	1340.41	< LOD	77.83	<lod< td=""><td>53.31</td><td>450.34</td><td>83.91</td><td>< LOD</td><td>109.36</td><td>< LOD</td><td>39.25</td><td>< LOD</td></lod<>	53.31	450.34	83.91	< LOD	109.36	< LOD	39.25	< LOD
B10.1	828.53	360.29	< LOD	105.44	<lod< td=""><td>68.54 <</td><td>< LOD</td><td>55.41</td><td>997715.13</td><td>861.21</td><td>< LOD</td><td>31.62</td><td><lod< td=""><td>26.11</td><td>< LOD</td><td>37.25</td><td>< LOD</td><td>52.87</td><td>< LOD</td><td>19.2</td><td>< LOD</td></lod<></td></lod<>	68.54 <	< LOD	55.41	997715.13	861.21	< LOD	31.62	<lod< td=""><td>26.11</td><td>< LOD</td><td>37.25</td><td>< LOD</td><td>52.87</td><td>< LOD</td><td>19.2</td><td>< LOD</td></lod<>	26.11	< LOD	37.25	< LOD	52.87	< LOD	19.2	< LOD
B10.2	792.18	8 394.93 < LOD	< LOD	110.82 < LOD	≺LOD	> 76.94	< LOD	59.31	997953.75	938.02 < LOD	< LOD	32.94	32.94 < LOD	23.23	< LOD	39.07	< LOD	53.08 < LOD	< LOD	19.94 <	< LOD
B10.3	17. 606	1 484.74 < LOD	4 LOD	138.41 < LOD	≺LOD	93.06 < LOD	ίου	73.73	998311.88	1118.9 < LOD	< LOD	38.19	38.19 < LOD	28.03	< 10D	49.16	49.16 < LOD	72.67 < LOD	< LOD >	25.24 < LOD	ГОР
C01.1	388.42	2 256.48 < LOD	Q0 ×	75.3	75.3 < LOD	48.59 < LOD	, LOD	40.75	997571.56	583.43 < LOD	<pre>COD </pre>	19.99	19.99 < LOD	14.94	< 10D	16.46	16.46 < LOD	22.37 < LOD	<pre>COD </pre>	11.27 < LOD	DD LOD
C01.2	401.67	7 264.56 < LOD	4 LOD	62	79 < LOD	53.77 < LOD	, LOD	41.35	998184.88	612.66	Q01 ≻	20.56	20.56 < LOD	9.91	< LOD	18.31	Q01 ≻	25.65 < LOD	Q01×	8.78	4 LOD
CO1.3	00 Y		Q01×	63.8	63.8 < LOD	42.64 < LOD	ίοD	34.05	998213.13	503.9	COD ×	14.32	14.32 < LOD	11.12	< LOD	12.93	4 LOD	61	19 < LOD	8.58	< LOD
C02.1	553.51	293.09	4 LOD	85.21	< LOD >	55.95 <	COD >	45.28	998547.81	670.31	4 LOD	32.95	32.95 < LOD	18.09	295.12	30.41	COD ×	33.48	4 LOD	11.68 <	< LOD
C02.2	COD >	454.28 < LOD	4 LOD	87.07 < LOD	≺LOD	59.56 <	<pre>COD </pre>	47.54	998538.31	718.05 < LOD	< LOD	28.01	28.01 < LOD	16.75	112.91	24.22	QD >	36.34	<pre>COD </pre>	12.65 <	< LOD
C02.3	498.24	4 270.55 < LOD	< LOD	79.53 < LOD	< LOD	53.92 <	< LOD	40.13	998803.69	626.72 < LOD	< LOD	27.12	27.12 < LOD	16.2	130.38	22.23	< LOD	29.21 < LOD	< LOD	11.47 < LOD	LOD
C03.1	569.59	9 356.04 < LOD	<pre>COD</pre>	97.29 < LOD	< LOD	70.58 < LOD	ίοD	55.48	998864.38	789.12 < LOD	< LOD	30.13	30.13 < LOD	25.51	< LOD	30.05	LOD	43.34 < LOD	<pre>COD ></pre>	17.68 < LOD	ΠOD
C03.2	2277.11	1 1113.67 < LOD	<pre>COD </pre>	303.71 < LOD	۲OD	187.99 < LOD		145.46	996413.38	2515.77	COD ≻	128.04	128.04 < LOD	84.08	< 10D	149.75	4 LOD	203.25 < LOD	< LOD >	63.55 < LOD	ОО
C03.3	666.14	4 313.69 < LOD	4 LOD	91.58 < LOD	< LOD	63.49 < LOD	ίοD	48.12	998645.94	720.29	COD ≻	24.41	<10D ×	12.33	< LOD	28.02	4 LOD	38.23	< LOD	9.6	< LOD
C04.1	518.97	312.62	< LOD	92.26	< LOD	59.5 < LOD	ίου	49.2	998134.94	729.09	< LOD	15.98	dol⊳i	17.23	33.03	19.06	< LOD	37.26	< LOD	13.61 <	< LOD
C04.2	673.5	5 304.78 < LOD	4 LOD	88.05 < LOD	LOD	58.25 <	⊂ LOD	47.82	997921.81	702.39	COD ×	29.45	29.45 < LOD	20.62	< LOD	28.74	4 LOD	35.95	< LOD	14.94 -	< LOD
C04.3	571.92	2 306.57 < LOD	<pre>COD ></pre>	89.16 < LOD	< LOD ×	62.94 < LOD	ίοD	47.21	998690.5	711.11 < LOD	< LOD	25.8	25.8 < LOD	19.61	< LOD	26.93	26.93 < LOD	37.42 < LOD	< LOD	13.42 < LOD	DD.
C05.1	877.84	4 306.69 < LOD	< LOD	89.62 < LOD	< LOD	58.62 < LOD	, LOD	45.9	998685.81	671.14 < LOD	< LOD	19.39	19.39 < LOD	16.86 < LOD	< LOD	23.97	< LOD	34.47 < LOD	< LOD	12.43 < LOD	LOD
C05.2	520.54	4 305.41 < LOD	< LOD	87.52 < LOD	< LOD	59.99 < LOD	, LOD	45.87	998658.75	722.54 < LOD	< LOD	26.01	26.01 < LOD	14.79	< LOD	25.02	< LOD	33.69 < LOD	< LOD	12.31 < LOD	TOD
C05.3	812.12	2 427.92 < LOD	4 LOD	117.77 < LOD	LOD	78.77 < LOD	â	62.45	998407.69	955.96	4 LOD	33.34	<pre>COD </pre>	19.17	< LOD	39.2	4 LOD	54.76 < LOD	4 LOD	20.08	< LOD
C06.1	Q01 ≻	477.53	< LOD	91.73	4L0D	61.28 <	Q01≻	51.16	90. 606866	749.2	4 LOD	18.62	COD	21.72	< LOD	26.31	Q07 ×	38.49	< LOD	15.29 <	< LOD
C06.2	Q01≻	531.88 < LOD	Q07 ×	104.25	COD ^	66.89 <	COD ∧	56.08	998911.56	815.12	Q07∨	26.44	4LOD	25.76	< LOD	28.93	Q0 ×	42.24	4 LOD	19.24 -	< LOD
C06.3	< LOD	650.31 < LOD	< LOD	125	125 < LOD	86.52 <	< LOD	62.89	998503.25	1009.95	< LOD	32.45	32.45 < LOD	25.17	< LOD	41.33	< LOD	57.49 < LOD	< LOD	19.51	< LOD
C07.1	829.6	6 335.18 < LOD	4 LOD	95.19 < LOD	LOD	62.9 <	⊂ LOD	51.61	998275.06	774.19 < LOD	< LOD	23.25	23.25 < LOD	22.57	< LOD	31.48	31.48 < LOD	40.49 < LOD	<pre>COD ></pre>	15.32 < LOD	DD.
	C07.2 633.23	335.81 < LOD	< LOD	92.48 < LOD	< LOD	001 > 00.99	ίοD	50.58	998319.5	760.77	< LOD	21.25	21.25 < LOD	18.25	< LOD	27.3	< LOD	41.24 < LOD	< LOD	15.1	< LOD
	C07.3 516.73	8 330.57 < LOD	4 LOD	97.24 < LOD	LOD	66.28 < LOD	ΰ	52.85	998591.44	764.76	⊂ LOD	27.94	27.94 < LOD	15.29	< LOD	27.31	< LOD	39.53	< LOD	15.14 <	< LOD
	C08.1 1119.7	400.09	< LOD	110.85	<lod< td=""><td>75.12 <</td><td>< LOD</td><td>56.81</td><td>998350.31</td><td>899.67</td><td>< LOD</td><td>29.57</td><td>COD≻.</td><td>17.98</td><td>< LOD</td><td>38.4</td><td>< LOD</td><td>55.15</td><td>< LOD</td><td>15.49</td><td>< LOD</td></lod<>	75.12 <	< LOD	56.81	998350.31	899.67	< LOD	29.57	COD≻.	17.98	< LOD	38.4	< LOD	55.15	< LOD	15.49	< LOD
	C08.2 496.49	309.14	< LOD	86.35	4 LOD	58.99 <	COD >	45.99	998454.75	737.4	COD ×	28.94	28.94 < LOD	19.1	< LOD	26.06	4 LOD	37.16	< LOD	14.07 <	4 LOD
	C08.3 < LOD	558.24 < LOD	< LOD	105.79 < LOD	≺LOD	70.69 < LOD	, LOD	57.02	998828.5	833.73	< LOD	20.06	20.06 < LOD	25.41	< LOD	32.22	< LOD	47	47 < LOD	18.54 <	< LOD
C09.1	< LOD	531.47 < LOD	< LOD	100.89 < LOD	≺LOD	70.77 <	< LOD	57.73	998450.56	842.36 < LOD	< LOD	28.83	28.83 < LOD	16.03 < LOD	< LOD	29.18	29.18 < LOD	40.89 < LOD	< LOD	12.8 < LOD	TOD
C09.2	2266.18	8 932.74 < LOD	Q07∨	259.2 < LOD	LOD	154.34 < LOD		127.85	996322.19	1926.34 < LOD	4 LOD	83.14	83.14 < LOD	68.52	< LOD	115.67	Q0 √	159.41 < LOD	QD^	56.18 < LOD	9
C09.3	Q0 × LOD	504.75 < LOD	Q0 ×	96.28 < LOD	LoD^	65.38 < LOD	ĝ	51.84	90.700666	764.04	οŢ	27.32	27.32 < LOD	18.96	< LOD	26.91	۲ دول	40.79 < LOD	COD ~	14.86 -	< LOD
C10.1	752.97	354.26	<pre>COD </pre>	98.44	<pre>COD </pre>	63.76 < LOD	â	51.64	998619.06	835.33	4 LOD	27.96	COD ×	26.01	< LOD	30.54	Q0 × LOD	44.71	4 LOD	19.12 -	< LOD
C10.2	3057.33	1167.23	<pre>COD </pre>	283.49	¢LOD	205.32 <	COD ∧	146.31	996114.63	2428.69	Q07∨	108.87	COD>	89.97	< LOD	156.75	Q0 Y	232.17	4 LOD	66.24 -	4 LOD
. m	C10.3 < LOD	536.87 < LOD	QD V	101.17 < LOD	^{CO}	69.02 < LOD	ĝ	52.87	998091.44	837.95 < LOD	do] ^	25.26	25.26 < LOD	14.8	14.8 < LOD	29.81	29.81 < LOD	42.47 < LOD	COD^	14.3 < LOD	8

313.46 LOD 88.71 LOD 59.93 208830.25 727 LOD 25.56 LOD 15.54 706.78 LOD 137.79 LOD 94.73 LOD 70.14 998813.63 1092.63 LOD 45.76 LOD 16.2 443.73 LOD 85.44 COD 59.46 COD 45.22 998813.63 677.14 LOD 45.76 10.0 16.2 334.84 LOD 85.44 COD 63.69 COD 45.72 998815.5 763.36 LOD 11.35 21.75 334.84 LOD 98.24 COD 61.71 COD 46.57 998815.5 763.36 21.0D 21.75 479.15 LOD 92.71 COD 61.74 COD 48.57 740.3 20.05 21.05 21.75 4703 LOD 92.71 21.00 81.34 20.05 23.66 20.02 23.42 4703 LOD 81.34 LOD	.44 313.48 88.71 59.33 998830.25 727 25.56 100 15.54 706.78 <u td=""> 137.79 <u td=""> 94.73 <u td=""> 99.8813.63 1092.63 <u td=""> 45.76 <u td=""> 16.2 443.73 <u td=""> 137.79 <u td=""> 94.73 <u td=""> 70.14 998813.63 1092.63<<u td=""> 45.76<<u td=""> 100 16.2 443.73 <u td=""> 55.46<u td=""> 100 70.14 998813.69 677.14<<u td=""> 11.35<<u td=""> <u td=""> 10.33 443.73<<u td=""> <u td=""> 100 55.46<u td=""> 400 45.22 998813.69 677.14 100 11.35<<u td=""> <u td=""> 13.34 56 334.84<<u td=""> <u td=""> 96.8400 50.6 998855.5 763.36<u td=""> 20.00 32.55<<u td=""> 200 21.75</u></u></u></u></u></u></u></u></u></u></u></u></u></u></u></u></u></u></u></u></u></u></u></u>	
706.78 LUD 137.79 LUD 94.73 LUD 98.813.63 LUD2.63 LUD 45.76 LUD 443.73 85.44 85.44 85.44 100 59.46 45.22 998818.69 677.14 100 11.35 100 9.6 334.84 98.24 8100 63.69 40.6 99885.5 763.36 100 32.55 100 9.6 334.84 900 99.24 8100 63.69 80.6 99885.5 763.36 100 32.55 81.00 7.4 409 92.71 81.00 61.71 81.00 48.57 998714.5 740.3 2066 81.00 7.4 409 107 117.14 81.00 81.34 100 62.68 998603.06 933.67 200 26.83 81.00 35.06 81.00 35.06 81.00 35.66 81.00 35.66 81.00 35.66 81.00 35.66 81.00 35.66 81.00 35.66	C11.2 < LOD	
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<pre>< LOD 340.8 < LOD 69.3 < LOD 49.78 < LOD 38.13 991660.13 561.35 < LOD 119.37 < LOD 33.15 733613</pre>	340.8 < LOD 69.3 < LOD 49.78 < LOD 38.13 991660.13 561.35 < LOD 119.37 < LOD 33.15	
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I tear Looi Ho Error		Å	Au Fror	7.0	7n Frrar	3	Cu Error	in in	Mi Fror	Ŀ	Fe Fror	-	Cr Error	-	V Fror	1=	Ti Fror	-	CIError
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T-T/W	T30.5/ < LUU		732.4		2T'00	20:T2 < LUU	/#7697		60.022	9T'NNØ	TQ:2Q7	Ĭ			C'C/ #T	6T'0#9	40.U0		27/3/
A01-2	88.85 88.85	88.85 < LOD	139.24	257.35	69.56	69.56 < LOD	172.85	0 V	126.09	1231.04	224.2	117.12	36.56 < LOD	0 0	1022.68	914.43	77.33	1440.05	188.32
A01-3	82.38	82.38 < LOD	127.01	166.58	55.31	55.31 < LOD	133.89	< LOD	113.3	194.15	117.98	79.34	35.53 < LOD	< LOD	930.46	< LOD	72.42	< LOD	223.99
AD3.1	42.89	< LOD	65.99	< LOD	40.46	40.46 < LOD	83.68	< LOD	72.74	1779.61	175.38	74.8	25.28 < LOD	< LOD	674.78	547.48	44.99	18649.93	512.02
A03.2	58.64	< LOD	89.78	95.17	40.78	×רסם	110.98	< LOD	93.29	4663.02	306.7	79.18	25.02	< LOD	695.09	1543.55	73.22	6181.39	232.18
A03.3	61.57	< LOD	98.72	129.34	48.82	<lod< td=""><td>134.12</td><td>< LOD</td><td>112.36</td><td>6924.12</td><td>401.87</td><td>89.37</td><td>23.51</td><td>< LOD</td><td>727.76</td><td>1882.56</td><td>87.36</td><td>4159.72</td><td>187.64</td></lod<>	134.12	< LOD	112.36	6924.12	401.87	89.37	23.51	< LOD	727.76	1882.56	87.36	4159.72	187.64
A05-1	83.68	83.68 < LOD	121.75	79.72	43.77	43.77 < LOD	128.86	< 10D	109.2	< 10D	155.96	155.96 < LOD	47.94 < LOD	< LOD	749.78	< 10D	65.17	< 10D	198.86
A05-2	87.1	87.1 < LOD	124.86	79.68	42.83	42.83 < LOD	117.53	< LOD	108.95	287.91	118.03	118.03 < LOD	46.84 < LOD	< LOD	760.91	< LOD	65.81	< LOD	203.67
A05-3	126.41 < LOD	< LOD	185.86	121.49	63.3	63.3 < LOD	193.03	10D × LOD	165.43	< 10D	226.82	226.82 < LOD	57.21 < LOD	100	1038.13	108.83	53.98	< 10D	269.71
A06-1	72.23	72.23 < LOD	104.95	104.77	39.82	39.82 < LOD	108.46	4 LOD	93.49	166.35	93.47	65.45	30.24 < LOD	<pre>COD </pre>	762.34	< 10D	61.99	< 10D	190.89
A06-2	93.33	< LOD	139.4	< LOD	72.04	≺LOD	137.03	TOD >	124.45	313.91	133.66	< LOD	51.58	< LOD	828.99	< 10D	70.79	< 10D	217.73
A06-3	68.36	< LOD	103.67	139.25	42.39	≺LOD	108.02	4 LOD	88.09	2011.35	212.71	80.95	27.04	< LOD	643.16	6.808	58.26	677.34	154.51
A07-1	23.68	23.68 < LOD	33.24	164.26	21.33	21.33 < LOD	38.6	< LOD	30.56	792.37	74.63	23.85	14.23	< LOD	324.69	261.55	22.14	< 10D	73.23
AD7-2	21.63	21.63 < LOD	29.75	154.94	19.35	19.35 < LOD	33.97	<pre>COD </pre>	27.36	395.89	52.95	< LOD	20.53 < LOD	<pre>COD </pre>	292.43	256.08	20.8	484.26	49.65
A07-3	35.09	35.09 < LOD	53.28	169.33	29	29 < LOD	58.87	<pre>COD </pre>	49.73	1083.56	111.67	25.11	16.6	16.6 < LOD	447.63	256.37	27.83	< 10D	95.48
A08.1	99.53	99.53 < LOD	168.41	172.6	73	73 < LOD	199.21	< LOD	151.99	431.18	183.82	66.22	40.49 < LOD	< LOD	1316.13 < LOD	< LOD	82.69 < LOD	< LOD	249.46
A08.2	74.73	74.73 < LOD	127.51	175.8	58.84	<10D	161.86	< LOD	139.12	706.54	178.33	< 10D	53	< 10D	1018.05	< 10D	73.77	< 10D	220.31
A08.3	73.59	< LOD	112.35	236.5	56.58	×רסם	144.39	< LOD	107.05	808.84	169.06	6.99	32.43	< LOD	913.35	83.58	46.29	< LOD	196.21
A09.1	77.11	< LOD	123.35	107.23	52.97	×۲٥D	145.49	< LOD	124.31	227.27	129.82	< LOD	54.9	< LOD	994.62	< 10D	73.01	282.82	157.36
A09.2	81.19	81.19 < LOD	139.9	166.43	59.89	59.89 < LOD	167.06	< LOD	130.22	279.64	141.13	68.19	38.13 < LOD	< 10D	1066.91 < LOD	< LOD	77.51	< 10D	244.34
A09.3	141.13 < LOD	< LOD	219.65	142.73	83.76	83.76 < LOD	250.69	< LOD	216.79 < LOD	< LOD	301.13	71.26	46.99 < LOD	< LOD	1504.02 < LOD	< LOD	95.95 < LOD	< LOD	325.58
A11-1	75.63	75.63 < LOD	107.13	65.25	37.94	37.94 < LOD	113.14	< LOD	88.21 < LOD	< LOD	130.52	< LOD	45.87 < LOD	< LOD	742.29 < LOD	< LOD	60.12 < LOD	< LOD	189.29
A11-2	56.95	< LOD	85.64	87.52	34.03	<۲OD	92.23	< LOD	72.8	< 10D	112.07	45.12	26.21 < LOD	< LOD	619.8	< 10D	51.95	< 10D	162.85
A11-3	73.48	< LOD	109.58	129.32	44.37	<lod< td=""><td>110.33</td><td>< LOD</td><td>99.46</td><td>694.67</td><td>145.63</td><td>< LOD</td><td>42.24</td><td>< LOD</td><td>685.39</td><td>200.23</td><td>41.95</td><td>398.45</td><td>128.23</td></lod<>	110.33	< LOD	99.46	694.67	145.63	< LOD	42.24	< LOD	685.39	200.23	41.95	398.45	128.23
A13-1	65.86	< LOD	93.43	< LOD	50.57	<lod< td=""><td>111.85</td><td>< LOD</td><td>101.24</td><td>199.35</td><td>104.88</td><td>76.4</td><td>30.73</td><td>< LOD</td><td>918.62</td><td>< 10D</td><td>105.23</td><td>43491.59</td><td>1376.77</td></lod<>	111.85	< LOD	101.24	199.35	104.88	76.4	30.73	< LOD	918.62	< 10D	105.23	43491.59	1376.77
A13-2	41.55	41.55 < LOD	61.03 < LOD	< LOD	31.06	31.06 < LOD	69.44	COD ∧	62.41	189.89	72.32	41.9	22.88	653.1	427.58 < LOD	< LOD	81.96	19422.72	525.33
A13-3	31.5	31.5 < LOD	41.18	49.04	17.45	17.45 < LOD	47.55	00 V	41.67	1270.58	108.65	53.06	17.85	737.5	299.83	1012.95	55.07	7100.46	187.45
B01-1	164.26 < LOD	Q07×	289.57	235.42	109.44 < LOD	dol≻	311.53	Q × LO	264.22 < LOD	< LOD	281.14	< LOD	99.24 < LOD	C0D^	1541.67 < LOD	¢ LOD	133.97	776.47	316.17
B01-2	196.08 < LOD	<pre>COD </pre>	303.05	440.79	135.97	Q07≻	331.63	۹ ۲O	285.45	< LOD	333.73	113.91	70.64 < LOD	<pre>COD </pre>	1810.45	< LOD	145.6	1247.22	336.1
B01-3	186.65	<pre>COD </pre>	306.69	367.96	129.93	dol≻	340.06	COD ∧	273.39	< LOD	350.32	< LOD	105.94	< LOD	1660.47	<pre>COD </pre>	142.38	773.27	323.48
B04.1	84.45	< LOD	125.18	75.84	45.97	<lod< td=""><td>132.11</td><td>< LOD</td><td>103.43</td><td>< LOD</td><td>168.65</td><td>82.69</td><td>37.52</td><td>< LOD</td><td>875.5</td><td>< LOD</td><td>76.08</td><td>2092.5</td><td>192.09</td></lod<>	132.11	< LOD	103.43	< LOD	168.65	82.69	37.52	< LOD	875.5	< LOD	76.08	2092.5	192.09
B04.2	<u> 79.69</u>	79.69 < LOD	128.31 < LOD	< LOD	65.82	65.82 < LOD	140.87	COD >	114.74	< LOD	171.35	171.35 < LOD	56.63 < LOD	COD ^	922.71	< LOD	76.21	< LOD	257.61
B04.3	84.77	84.77 < LOD	129.03 < LOD	< LOD	70.95	70.95 < LOD	141.17	< LOD	114.81	< LOD	163.31	98.17	38.91 < LOD	< LOD	939.51	< LOD	78.59	347.28	173.14
B06.1	56.57	< LOD	91.53	106.41	44.27	44.27 < LOD	116.93	< LOD	89.85	< 10D	130.75	78.43	32.83 < LOD	< LOD	864.2	< LOD	64.79	< 10D	203.65
B06.2	63.77	< LOD	19.61	143.56	46.01	<lod< td=""><td>120.12</td><td>< LOD</td><td>98.21</td><td>201.63</td><td>104.88</td><td>94.13</td><td>33.61</td><td>33.61 < LOD</td><td>870.03</td><td>< LOD</td><td>65.43</td><td>< LOD</td><td>209.1</td></lod<>	120.12	< LOD	98.21	201.63	104.88	94.13	33.61	33.61 < LOD	870.03	< LOD	65.43	< LOD	209.1
B06.3	62.46	< LOD	104.62	137.34	47.76	≺LOD	122.52	< LOD	100.55	< LOD	151.07	55.29	34.98	< LOD	928.32	< LOD	68.86	421.96	143.53
B07.1	164.28	< LOD	259.67	368.05	112.22	≺LOD	281.08	< LOD	246.95	< LOD	332.83	154.33	66.95	< LOD	1425.13	< LOD	142.18	2589.65	359.23
B07.2	233.34 < LOD	< LOD	374.44	1121.15	211.6	211.6 < LOD	397.22	< LOD	326.4	< LOD	441.5	220.2	83.58	83.58 < LOD	1616.47	7445.07	530.85	1633.28	341.22
B07.3	162.36 < LOD	4 LOD	260.83	343.22	110.7	110.7 < LOD	293.4	293.4 < LOD	236.85	359.54	226.89	186.63	66.87 < LOD	¢ LOD	1494.13	192.27	94.9	3278.03	374.51

User Logi	Hg Error	Au	Au Error	Zn	Zn Error	3	Cu Error	ï	Ni Error Fe		Fe Error	L.	Cr Error	>	V Error	ب ۲	Ti Error	сі С	CLError
B08.1	9	00, ×	0	<pre>COD</pre>	69.61	<pre>COD </pre>	176.05	۲ وا	139.78	322.31	146.73	139.41	92	< LOD ×	1089.98	Q01 ×	89.86	2180	214.27
B08.2	71.92	< LOD >	115.87	< LOD	62.01	62.01 < LOD	136.36	TOD >	1.901	209.5	124.52	67.29	39.1	39.1 < LOD	1019.87	< LOD	76.04	1625.69	169.82
B08.3	116.56 < LOD	< LOD	183.48 < LOD	< LOD	84.48	84.48 < LOD	206.72	< LOD >	176.76 <1	< LOD	263.04	82.73	52.42	52.42 < LOD	1302.6	< LOD	107.42	2069.7	253.84
B09.1	218.06 < LOD	< LOD	343.5	255.62		122.68 < LOD	359.75	< LOD	312.68 < 1	< LOD	392.14	208.69	81.83	81.83 < LOD	1704.38	1141.14	149.21	4498.32	485.98
B09.2	137.86 < LOD	< LOD	227.07	235.97	92.42	92.42 < LOD	256.78	< LOD	220.4 < 1	< LOD	285.37	103.79	62.58	62.58 < LOD	1335.55	2105.41	161.22	712.54	277.24
B09.3	211.95	< LOD	346.9	289.78		131.96 < LOD	375.44	< LOD	302.01 < 1	< LOD	394.27	141.84	77.64	< LOD	1645.15	1848.35	182.64	< LOD	493.05
B10.1	103.54	< LOD	167.87	451.95	87.88	< LOD	169.95	< LOD	149.34	378.73	158.27	103.36	45.07	< LOD	1071.96	< LOD	90.03	< LOD	296.69
B10.2	109.42 < LOD	< LOD	173.01	436.42		89.78 < LOD	179.41	Q01 ×	159.44 < 1	< LOD	205.48	108.7	47.3	< LOD	1182.29	< LOD	96.39	< LOD	300.75
B10.3	134.42 < LOD	< LOD	222.44	342.21		100.49 < LOD	246.52	< LOD	197.78	< LOD	263.91	91.81	52.2	52.2 < LOD	1390.89	< LOD	106.27 < LOD	< LOD	355.54
C01.1	45.98	45.98 < LOD	70.72	135.85		39.98 < LOD	1001	< LOD	76.62	401.52	112.88	54.17	26.62	26.62 < LOD	757.21	936.06	54.76	440.63	103.47
C01.2	50.55	50.55 < LOD	80.45	135.18		41.25 < LOD	101.71	< LOD	81.39	207.69	97.53	56.19	27.22	27.22 < LOD	796.68	869.29	53.94	< LOD	153.1
C01.3	34.9	< LOD	59.27	174.25		35.46 < LOD	- 27.66	< LOD	63.6	301.14	86.02	76.5	23.46	< LOD	652.69	982.4	48.5	< 10D	124.08
C02.1	59.44	< LOD	105.67	282.01	57.34	< LOD	116.31	< LOD	90.51 < 1	< LOD	152.02	122.54	32.29	< LOD	838.99	< LOD	64.04	< LOD	200.34
C02.2	69.44	< LOD	116.81	298.73		61.87 < LOD	132.94	< LOD	105.46	451.14	138.75	82.97	36.42	< LOD	889.03	< LOD	78.43	< LOD	227.68
C02.3	58.01	58.01 < LOD	93.79	244.43		52.09 < LOD	110.56	< LOD	85.48 < 1	< LOD	138.32	67.28	31.16	31.16 < LOD	786.61	< LOD	60.93 < LOD	< LOD	193.16
C03.1	83.37	83.37 < LOD	137.87	267.65		66.21 < LOD	152.81	< LOD	126.14 < 1	< LOD	183.63	< LOD	62.2	62.2 < LOD	966.59 < LOD	< LOD	82.14	< LOD	263.89
C03.2	410.04 < LOD	< LOD	624.78	< LOD	298.64	298.64 < LOD	670.25	< LOD	569.9 < LOD	LOD	678.64 < LOD	< LOD	146.3 < LOD	< LOD	3106.5	< LOD	209.4 < LOD	< LOD	786.32
C03.3	77.41	< LOD	123.05	234.66		60.4 < LOD	141.93	< LOD	106.11 < 1	< LOD	166.36	124.06	37.74	< LOD	899.21	< LOD	74.41	< LOD	231.68
C04.1	68.93	< LOD	117.47	287.53		62.18 < LOD	133.64	< LOD	107.29	277.79	123.69	90.6	35.76	< LOD	928.7	< LOD	71.7	521.17	150.89
C04.2	70.12	< 10D	112.59	352.99	65.87	<lod -<="" td=""><td>129.66</td><td>< LOD</td><td>111.32</td><td>183.94</td><td>114.85</td><td>111.54</td><td>35.85</td><td>< LOD</td><td>891.93</td><td>< 10D</td><td>71.41</td><td>560.83</td><td>150.93</td></lod>	129.66	< LOD	111.32	183.94	114.85	111.54	35.85	< LOD	891.93	< 10D	71.41	560.83	150.93
C04.3	75.89	75.89 < LOD	119.97	279.82		62.22 < LOD	135.09	< LOD	103.94 < 1	< LOD	152.03	80.22	36.14	36.14 < LOD	892.21	< LOD	71.47	< LOD	232.65
C05.1	62.03	62.03 < LOD	107.82	235.62		56.92 < LOD	126.19	< LOD	101.14 < 1	< LOD	139.8	64.36	33.49	33.49 < LOD	842.56 < LOD	< LOD	65.97	< LOD	196.97
C05.2	66.81	66.81 < LOD	107.4	264.96		57.64 < LOD	126.16	< LOD	101.15	248.89	113.94	65.05	36.04	36.04 < LOD	916.46	< LOD	71.9	< LOD	217.39
C05.3	105.67	< LOD	172.95	208.89		73.85 < LOD	196.02	<pre>COD ></pre>	154.14 < 1	< LOD	236.13	107.72	42.38	< LOD	1193.88	< LOD	86.08	< LOD	274.88
C06.1	72.53	< LOD	123.89			62.52 < LOD	135.81	Q01 ×	104.31	243.94	125.79	72.02	37.84	< LOD	933.88	< LOD	76.72	< LOD	243.3
C06.2	79.88	< LOD	134.08	362.31	73.44	73.44 < LOD	148.17	Q0 ×	128.82 < 1	< LOD	164.73	117.8	42.79	< LOD	1012.14	< LOD	84.58	< LOD	279.61
C06.3	114.56 < LOD	< LOD	183.18	333.11	85.72	85.72 < LOD	196.76	Q0 × LOD	170.55 < 1	< LOD	224.79	< LOD	74.71	74.71 < LOD	1262.16	< LOD	100.68	< LOD	325.02
C07.1	83.49	83.49 < LOD	127.15	302.38		67.38 < LOD	148.14	4 LOD	110.11	287.3	135.09	10.67	37.96	37.96 < LOD	966.86	< LOD	76.5	< LOD	240.29
C07.2	74.74	74.74 < LOD	130.24	329.96		68.41 < LOD	143.73	۲ ۲	116.91	413.65	144.06	99.16	37.95	37.95 < LOD	937.87	< LOD	76.61 < LOD	COD ×	243.79
C07.3	74.52	74.52 < LOD	121.96	278.52		64.4 < LOD	145.26	0 V	118.42	332.12	136.61	90.61	37.95	< LOD	947.44	< LOD	76.29	10D	238.8
C08.1	107.55	< LOD >	173	256.31	77.45	77.45 < LOD	189.44	Q v	163.31 < 1	< LOD	190.01	77.88	46.36	< LOD	1123.84	< LOD	92.28	< LOD <	288.6
C08.2	72.74	< LOD	119.67	305.46		62.96 < LOD	130.08	QO1 ≻	104.91	258.98	121.09	68.19	36.12	< LOD	938.86	< LOD	6.07	302.47	153.09
C08.3	88.97	< LOD	142.88	282.77	68	< LOD	157.46	< LOD	124.29 < 1	< LOD	177.06	89.05	43.97	43.97 < LOD	1030.9	< LOD	86.52	< LOD	269.22
C09.1	81.13	81.13 < LOD	128.65	346.26		71.07 < LOD	150.2	Q0 ≻	123.23 < 1	< LOD	184.06	112.59	39.31	39.31 < LOD	1074.58 < LOD	< LOD	81.2	364.65	173.13
C09.2	315.4	315.4 < LOD	501.97	< LOD	253.9	253.9 < LOD	561.67	Q01 ×	497.8 < 1	< LOD	563.79	< LOD	113.76 < LOD	< LOD	2271.42	< LOD	160.56	< LOD	603.56
C09.3	75.11	75.11 < LOD	127.68	322.2		65.85 < LOD	143.06	Q0 × LOD	119.04 < 1	< LOD	155.97	< LOD	58.77 < LOD	< LOD	944.41	< LOD	77.48	< LOD	242.13
C10.1	85.12	< LOD	138.66	278.15	67.78	< LOD	150.9	< LOD	117.46 < 1	< LOD	175.14	< LOD	64.55	< LOD	1060.14	< LOD	84.27	< LOD	265.35
C10.2	423.7	<pre>COD </pre>	700.3	< LOD	344.27	<pre>COD </pre>	704.76	Q LOD	647.09 < 1	< LOD	673.68	< LOD	162.11	< LOD	2910.03	< LOD	229.27	< LOD	854.87
C10.3	83.29	162.15	88.22	328.64		70.15 < LOD	158.49 <	< LOD	117.8	254.19	133.88	125.32	42.78	42.78 < LOD	1053.21 < LOD	< LOD	86.66	321.07	187.82

User Logi Hg Error		Au	Au Error	Zn Z	Zn Error	3	Cu Error h	z z	Ni Error	Fe	Fe Error	C.	Cr Error	>	V Error	1=	Ti Error	CI C	CIError
C11.1	71.05	< TOD >	115.45	196.34	55.38	55.38 < LOD	129.57 <	4 LOD	105.88	< LOD	161.88	< LOD	57.37	<pre>COD</pre>	914.89	< LOD	76.33	< LOD	237.14
C11.2	128.05 < LOD	< LOD	206.04	196.36	81.29	81.29 < LOD	225.86 < LOD	ίου	182.97	< LOD	223.1	< LOD	72.47 < LOD	< LOD	1373.09 < LOD	< LOD	99.22 < LOD	< LOD	308.61
C11.3	59.66	59.66 < LOD	101.51	305.72	55.63	55.63 < LOD	114.62	< LOD	96.12	193.08	98.44	70.1	32.54 < LOD	< LOD	849.33 < LOD	< LOD	63.54 < LOD	< LOD	203.35
C12.1	74.6	74.6 < LOD	120.54	281.14	63.79	63.79 < LOD	137.75 <	< LOD	117.79	< LOD	157.97	86.95	39.09	< LOD	950.61 < LOD	< LOD	77.26	< LOD	252.78
C12.2	73.45	< LOD	116.43	310.28	63.8	63.8 < LOD	135.25	< LOD	105.13	260.19	121.7	94.7	35.78	< LOD	926.82	< LOD	71.84	< LOD	226.43
C12.3	106.41	< LOD	161.79	230.19	73.4	73.4 < LOD	200.18	< LOD	155.05	< LOD	194.24	< LOD	63.73	< LOD	1172.34	< LOD	82.75	< LOD	270.73
C13.1	69.25	69.25 < LOD	109.85	224.89	57.35	57.35 < LOD	128.54 <	< LOD	108.37 < LOD	< LOD	157.67	122.31	36.07 < LOD	< LOD	907.48 < LOD	< LOD	70.56 < LOD	< LOD	224.62
C13.2	144.02 < LOD	< LOD	229.95	215.36	93.87	93.87 < LOD	271.48 < LOD	¢ LOD	225.27	< LOD	251.82	< LOD	73.81 < LOD	< LOD	1625.88 < LOD	< LOD	100.61 < LOD	< LOD	336.11
C13.3	71.72	71.72 < LOD	117.37	202.56	56.48	56.48 < LOD	138.42 < LOD	(LOD	116.09	191.24	118.61	74.64	36.13 < LOD	< 10D	979.32 < LOD	< LOD	72.73	72.73 < LOD	223.07
C14.1	45.7	45.7 < LOD	74.27	154.34	39.59	39.59 < LOD	94.45 < LOD	, LOD	69.15	622	120.62	52.54	26.02	26.02 < LOD	735.15 < LOD	< LOD	51.56 < LOD	< LOD	147.74
C14.2	38.18	65.11	41.23	158.94	34.9	34.9 < LOD	76.49 <	< LOD	60.02	290.29	86.57	79.28	23.99	< LOD	640.39	< LOD	46.03	< LOD	132.61
C14.3	47.15	< LOD	72.97	130.4	38.78	38.78 < LOD	97.52 <	< LOD	75.03	557.13	118.85	81.45	26.95	< LOD	721.09	69.45	36.86	302.44	106.78
C15.1	57.08	< LOD	83.08	119.85	36.2	36.2 < LOD	92.15	< LOD	77.41	500.57	113.51	< LOD	42.07	< LOD	581.19	129.55	40.31	372.91	118.06
C15.2	48.33	48.33 < LOD	73.07	158.91	35.88	35.88 < LOD	77	< LOD	63.21	155.82	73.44	40.42	26.21 < LOD	< LOD	518.96	< LOD	52.45	243.59	108.4
C15.3	64.6	64.6 < LOD	90.61	141.04	38.63	38.63 < LOD	94.02 < LOD	, LOD	81.63	1178.63	161.97	89.74	29.33 < LOD	< LOD	621.03	162.72	42.89	23205.76	725.52
C15e-1	83.15	83.15 < LOD	137.87	440.84	78.76	78.76 < LOD	155.8 < LOD	, LOD	128.27	996.38	196.24	69.95	39.51 < LOD	< LOD	964.56	311.67	60.45	1849.72	191.15
C15e-2	120.43 < LOD	< LOD	201.51	282.07	88.91	88.91 < LOD	226.72	< 10D	177.8	1308.98	276.1	< 10D	72.37 < LOD	< 10D	1174.45	521.38	77.32	1483.66	221.02
C15e-3	720.81 < LOD	< LOD	1162.82	< LOD	557.18 < LOD	< LOD	1293.22	< LOD	1106.32	5861.97	1425.76	< LOD	200.92	< LOD	3160.89	1180.72	273.58	< LOD	1038.54
C16.1	56.52	< LOD	80.48	143.56	35.71	<lod< td=""><td>84.04 <</td><td>< LOD</td><td>70.82</td><td>422.4</td><td>101.15</td><td>68.37</td><td>27.67</td><td>< LOD</td><td>558.07</td><td>70.27</td><td>39.63</td><td>495.66</td><td>117.75</td></lod<>	84.04 <	< LOD	70.82	422.4	101.15	68.37	27.67	< LOD	558.07	70.27	39.63	495.66	117.75
C16.2	76.38	< LOD	104.26	147.92	44.87	123.92	> 13	< LOD	93.85	161.02	94.23	< LOD	49.77	< LOD	688.41	< LOD	66.06	< LOD	201.55
C16.3	80.64	80.64 < LOD	114.08	133.75	46.06	46.06 < LOD	112.82	< LOD	89.83	205.56	102.19	< 10D	48.35 < LOD	< LOD	743.48 < LOD	< LOD	63.86 < LOD	< LOD	194.01
C17.1	104.44 < LOD	< LOD	161.62	< LOD	81.17	81.17 < LOD	169.72 < LOD	(LOD	143.52	374.05	156.85	73.3	40.94 < LOD	< LOD	946.75 < LOD	< LOD	83.77	83.77 < LOD	266.53
C17.2	67.61	67.61 < LOD	108.17	95.66	42.8	42.8 < LOD	123.04 < LOD	, LOD	97.82	1144.21	180.13	60.56	33.63 < LOD	< LOD	732.83	297.3	52.16 < LOD	< LOD	214.99
C17.3	102.77 < LOD	< LOD	164.06	122.44	57.94	57.94 < LOD	169.55 <	< LOD	138.93	308.14	146.38	< LOD	67.47 < LOD	< LOD	928.33	< LOD	89.07	< LOD	295.66
C18.1	57.01	< LOD	75.34	145.13	35.99	35.99 < LOD	87.57 <	< LOD >	72.09	548.44	112.57	52.95	27.29	< LOD	578.41	< LOD	57.53	194.47	112.52
C18.2	84.2	< LOD	123.3	131.36	47.77	×۲٥D	122.5 <	< LOD	114.33	166.06	104.52	< LOD	48.4	< LOD	792.44	< LOD	66.23	< LOD	216.42
C18.3	44.93	44.93 < LOD	64.67	110.83	28.87	28.87 < LOD	67.38 <	< LOD	55.5	216.23	71.48	64.22	24.26	24.26 < LOD	459.26	60.44	32.85	299.6	95.85
C19.1	51.7	51.7 < LOD	77	212.57	40.4	40.4 < LOD	81.1 <	Q01 ≻	69.07	482.19	103.61	70.26	26.24 < LOD	Q01×	549.14	132.09	38.47	< LOD	165.19
C19.2	121.37 < LOD	< LOD	170.39	220.42	66.74	66.74 < LOD	165.57 <	00 V	136.95	< LOD	172.11	78.18	40.53 < LOD	Q07×	944.47	< LOD	86.07	< LOD	255.01
C19.3	44.94	44.94 < LOD	63.82	220.61	38.23	38.23 < LOD	77.74 <	COD × LOD	63.58	625.13	108.13	57.77	24.25	24.25 < LOD	521.15	221.46	36.79	280.52	100.74
C20-1	68.93	68.93 < LOD	101.46	162.83	46.52	46.52 < LOD	111.53	< LOD	86.86	534.72	131.26	51.45	28.85	< LOD	721.12	153.84	42.11	1037.83	128.23
C20-2	65.31	< LOD	95.44	202.45	45.96	45.96 < LOD	99.55 <	< LOD	80.81	165.12	88.89	< LOD	43.87	< LOD	629.87	< LOD	59.83	< LOD	178.49
C20-3	70.07	70.07 < LOD	106.61	227.14	49.65	49.65 < LOD	103.26 < LOD	ίοD	89.36	468.5	120.4	63.71	30.46 < LOD	4 LOD	641.48 < LOD	< LOD	64.42 < LOD	< LOD	190.55